

What Does the Future Hold for Transformers and Inductors in Medium and High Power Applications

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ISO9001:2015
ISO13485 2016



Medium to High Power Magnetics

Power levels increasing to 10 kW and higher.

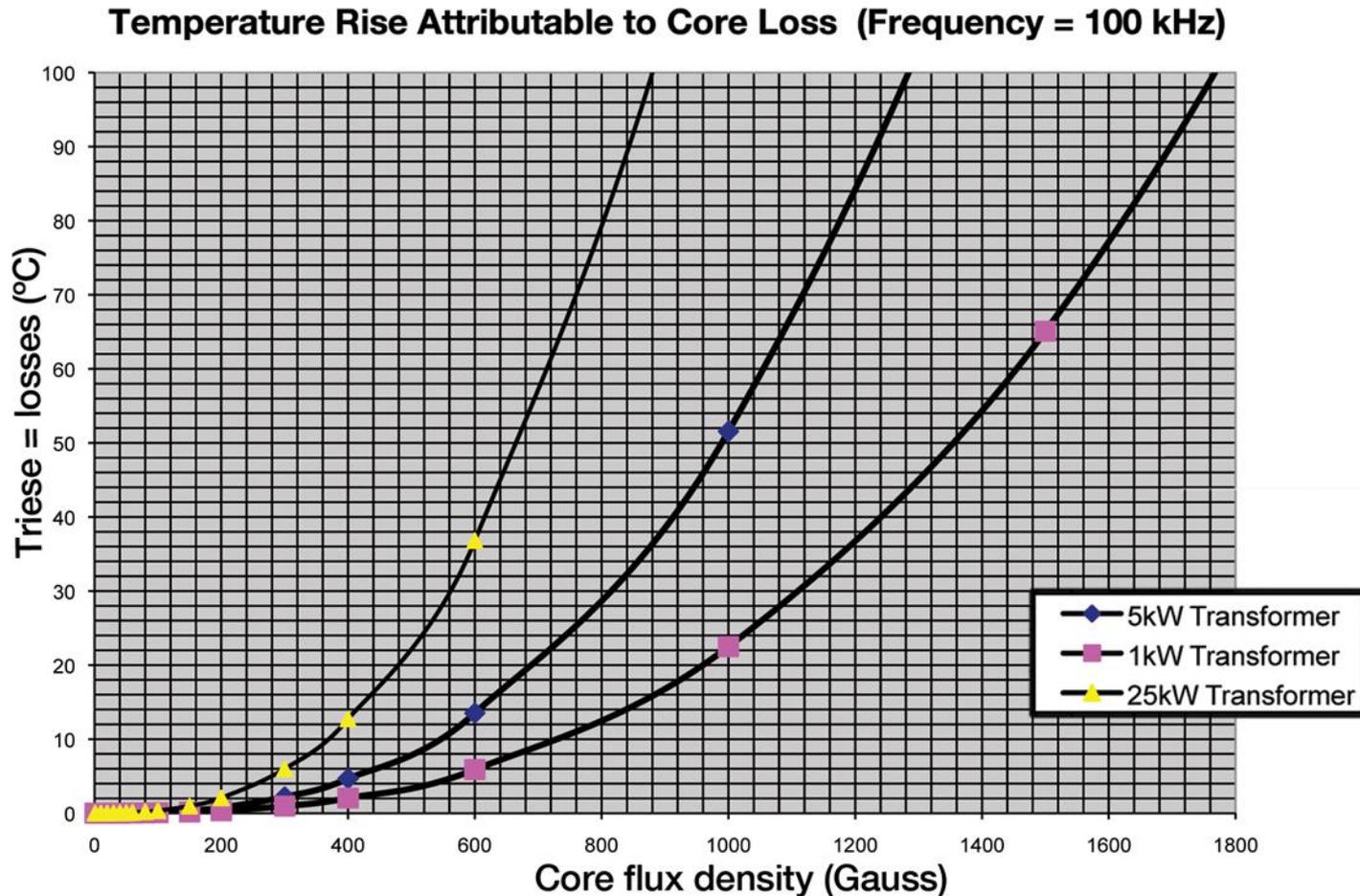
Frequencies increasing beyond 100 kHz to 500 kHz

LLC resonant circuits becoming common

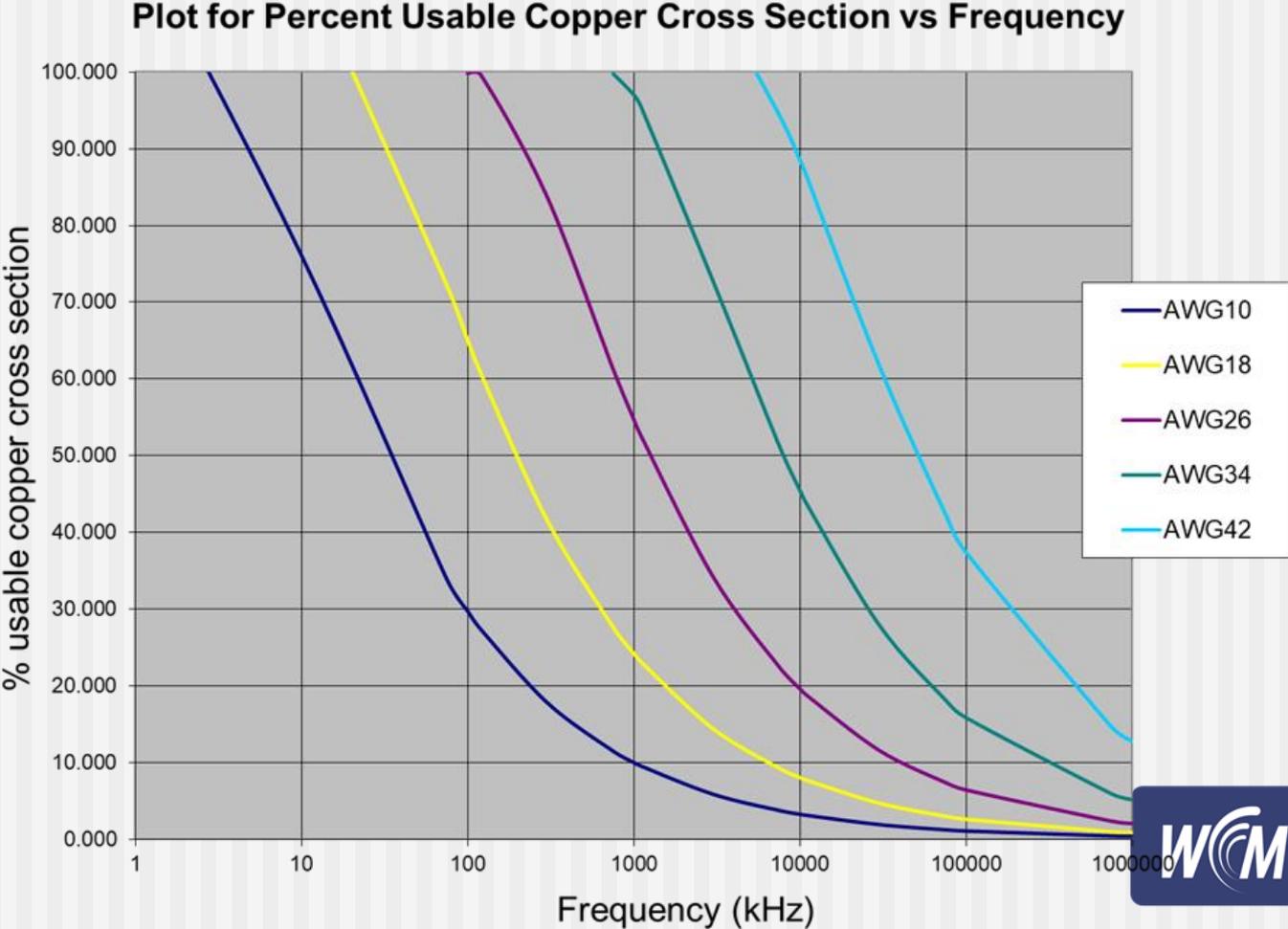
OUTLINE

- Highlight challenges
- 7 kW transformer design example
- Ferrites for higher frequencies
- Inductors for medium, high power

Larger Geometries Inherently Have Tendency to Higher Temperature Rise

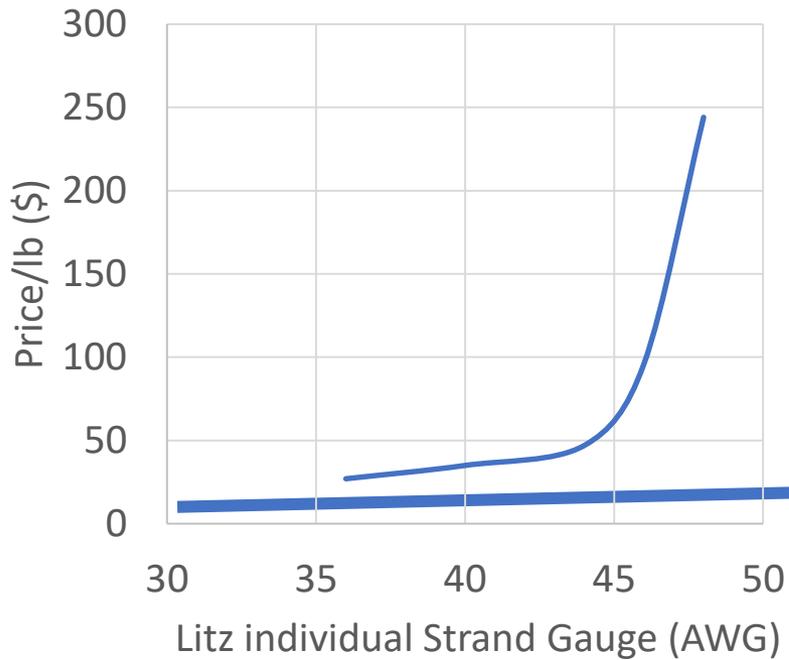


Higher Currents Require Design for AC Resistance Minimization

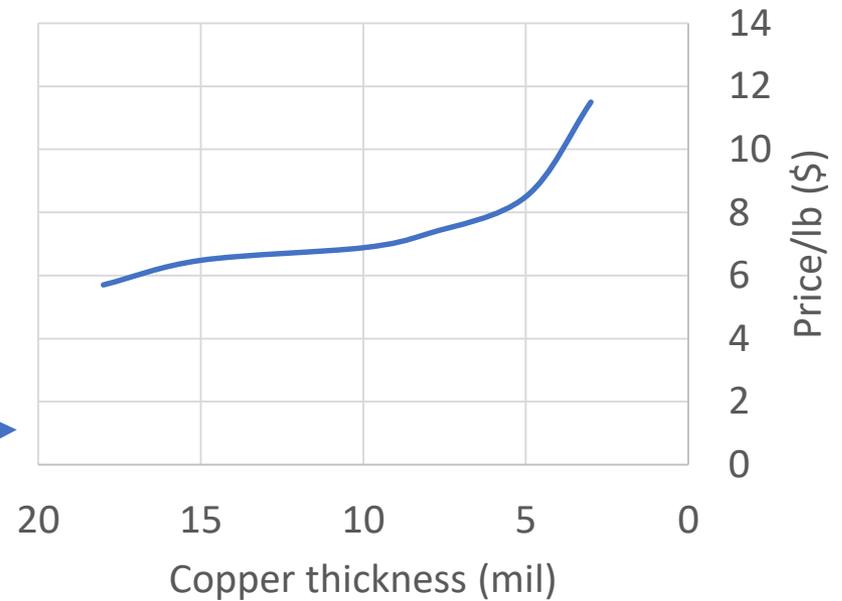


Cost of Litz Wire and Copper Foil

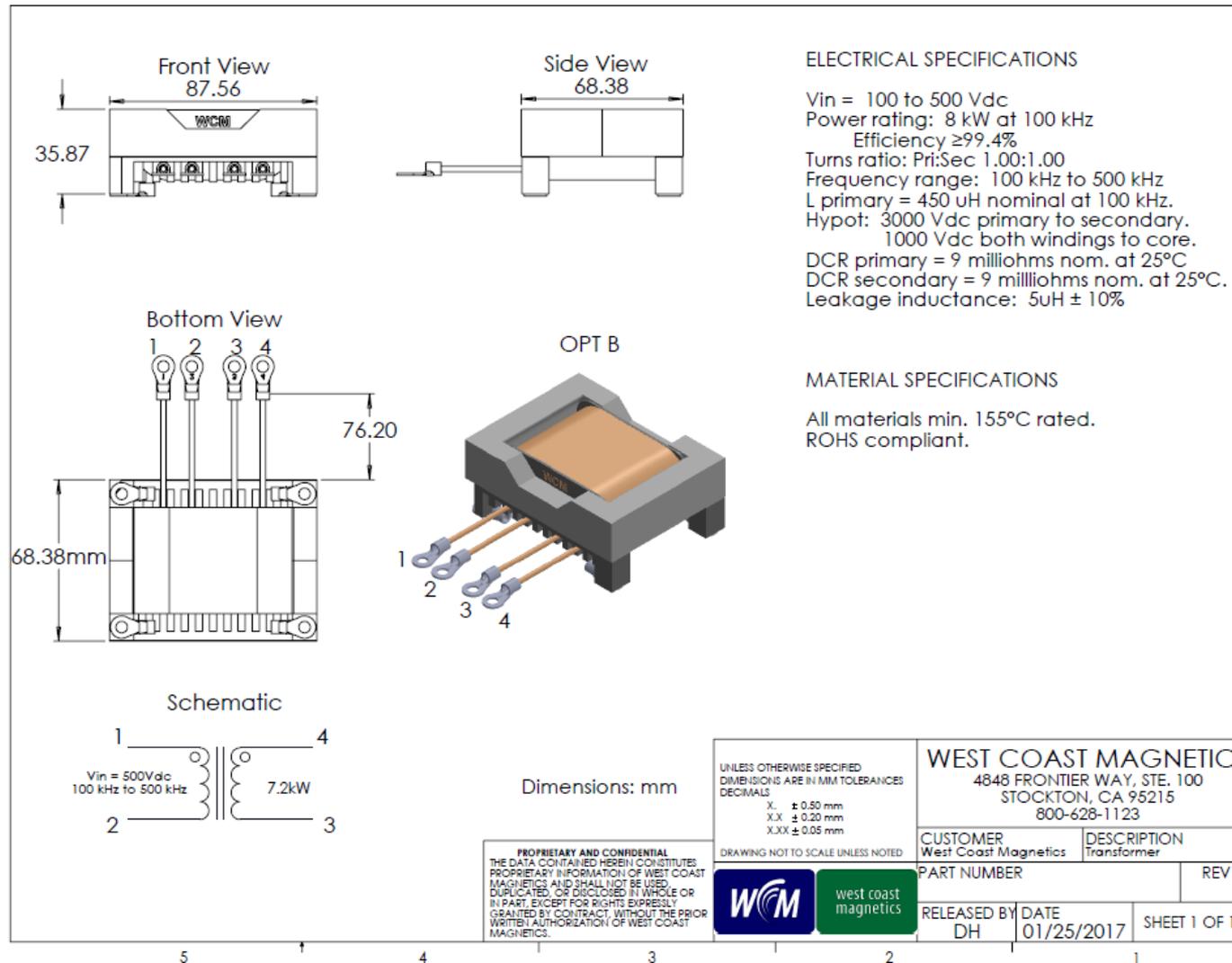
Litz Wire Price/lb versus AWG



Copper foil Price/lb versus thickness



TRANSFORMER DESIGN EXAMPLE

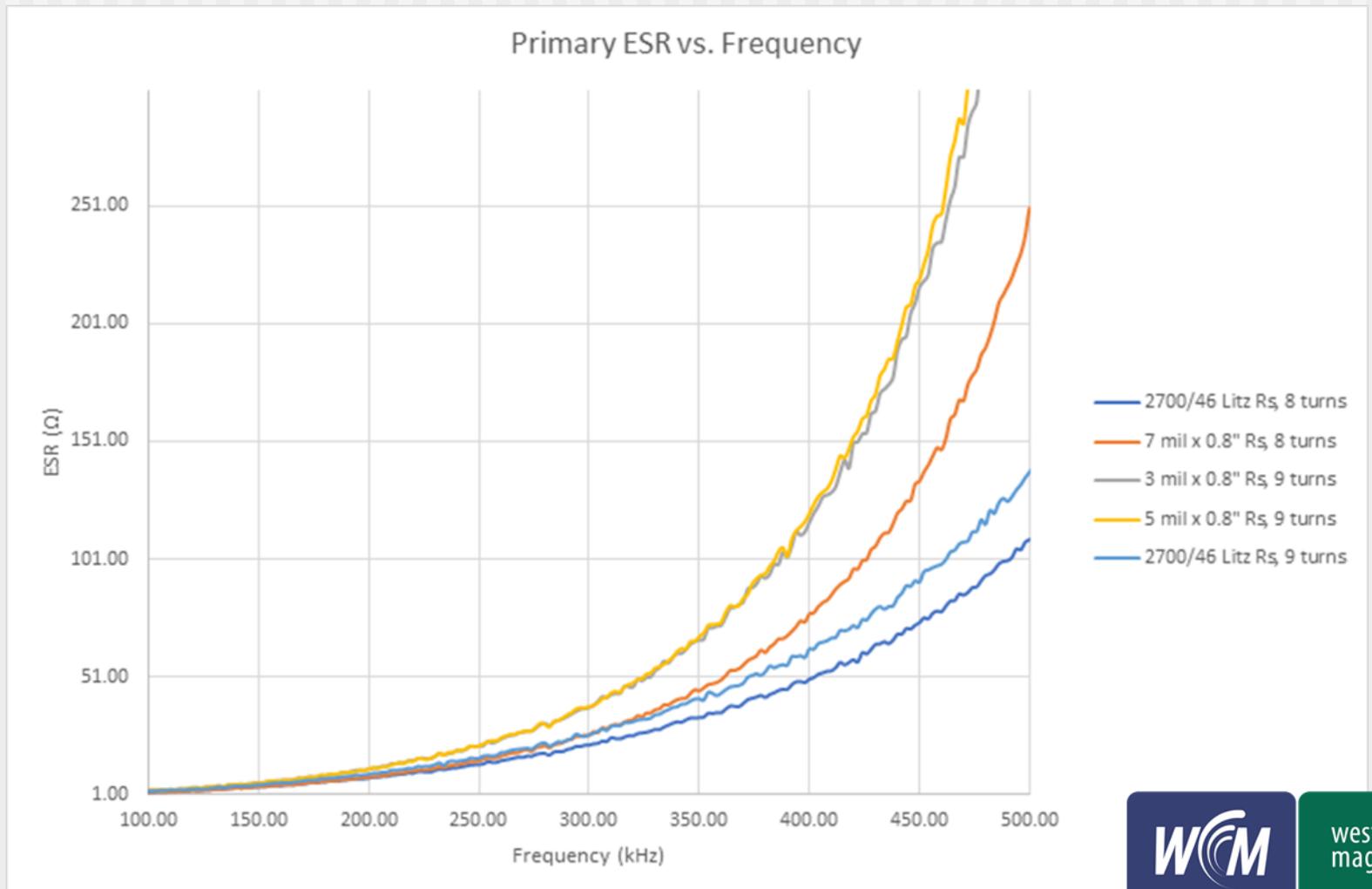


Design Elements – 7 kW SMPS Transformer

- New WCM410-88 core
- Potting to thermally couple bobbin and core
- 155 C materials
- Use of ferrite tape for leakage layer
- Shape opt optimization
- Investigation of foil
- Foil leakage layer



Loss Measurement for Different Windings



Performance Factor - Core

$$AN = \frac{E_{rms}(10^8)}{4.44Bf}$$

Where :

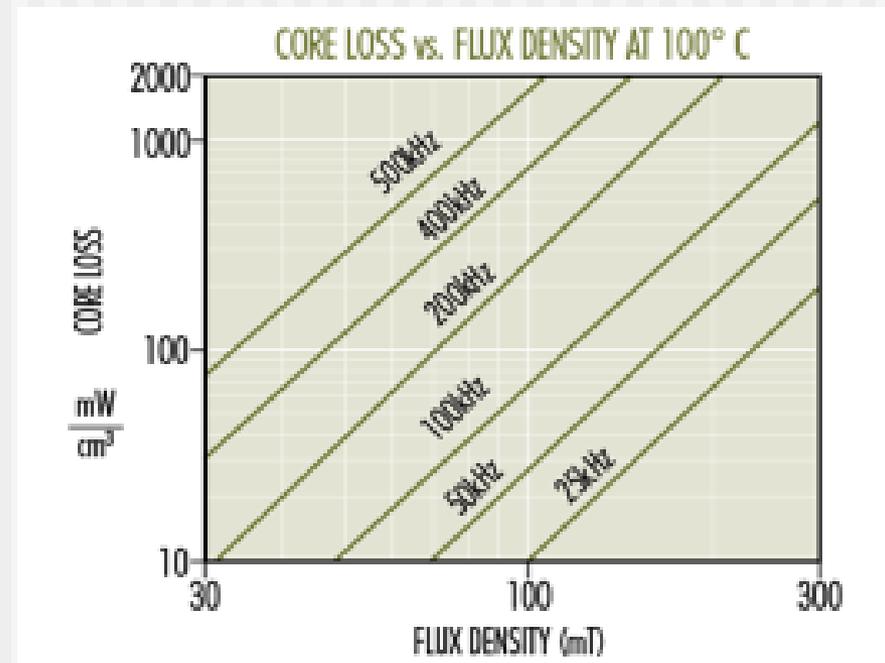
B = peak AC flux density (gauss)

E_{rms} = rms primary voltage

A = core area, (cm²)

N = number of primary turns

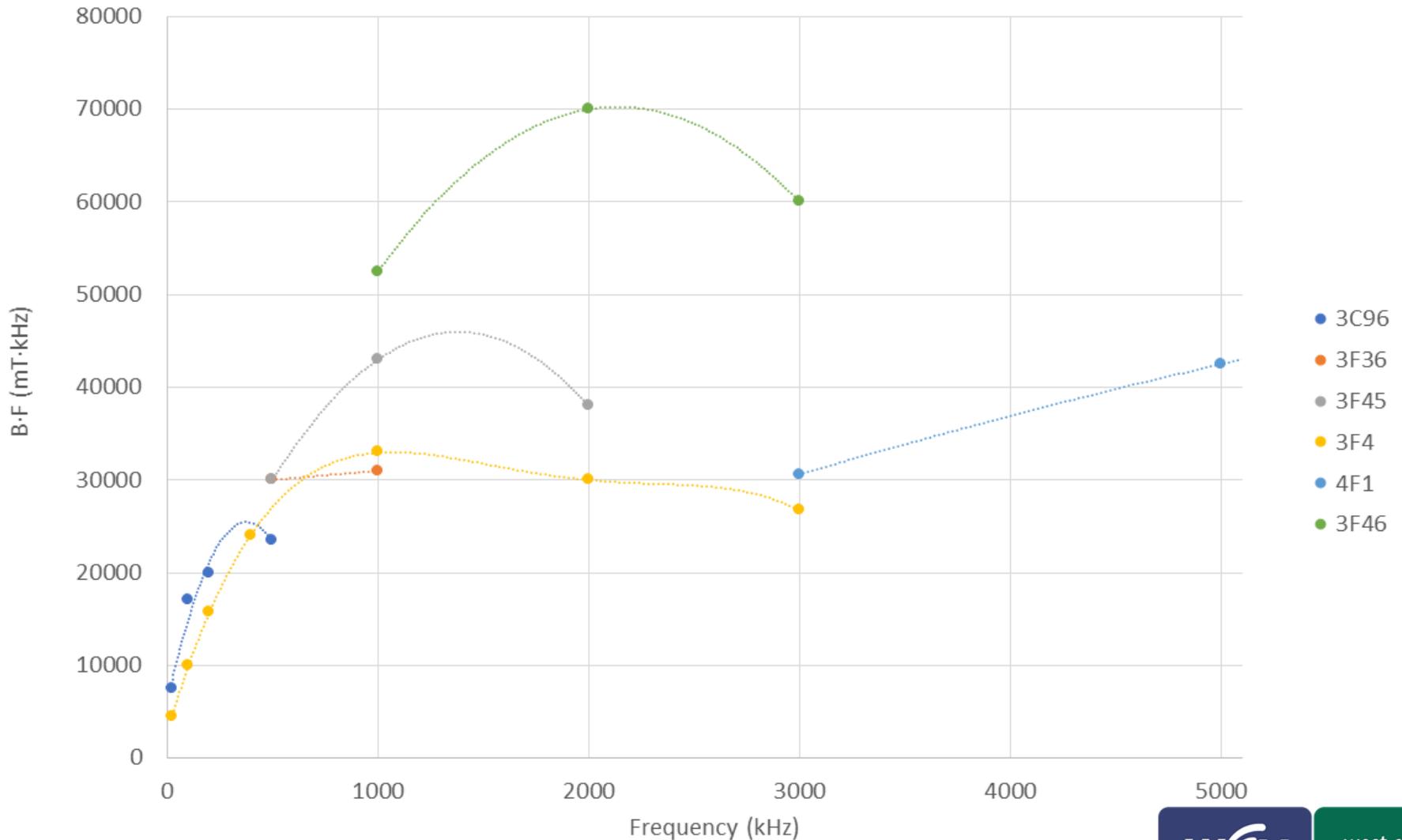
f = operating frequency



To reduce the size of our transformer we want to find a better material that will allow us to increase the value of B while holding the frequency and core loss density constant. This enables the use of less turns (lower winding resistance) and a smaller core.

BF Product for MnZn Ferrites

B·F vs. Frequency - Ferroxcube



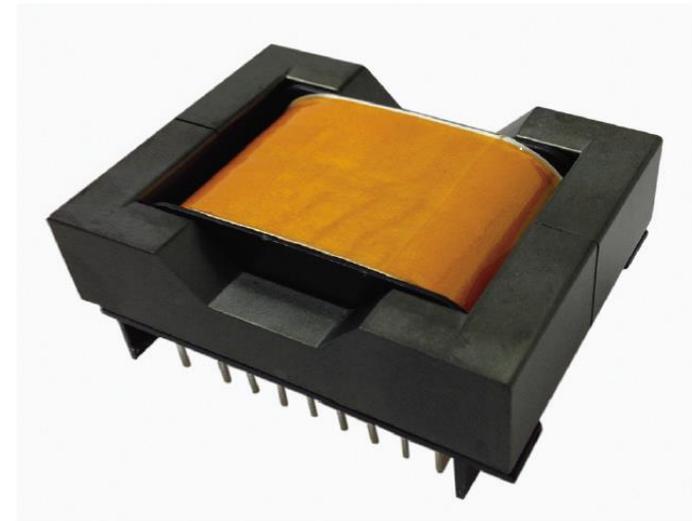
Inductors

- Must consider saturation in addition to core loss
- Inductor size, cost, loss dependent on L value and associated ripple
- Most designs are still powdered toroids until power levels are very high.
- At high power levels we are seeing more topologies using transformer leakage L for the inductor.
- More designs are requiring ferrite cores due to higher frequency and ripple requirements
- Gap effects create loss in ferrite based designs

WCM Shaped Foil Inductors

Low loss gapped ferrite core, shaped foil winding.

<i>Product Code</i>	<i>Inductance (μH) $\pm 10\%$</i>	<i>DCR ($\text{m}\Omega$)</i>	<i>idc amps INPUT</i>	<i>Schematic</i>
WCM319-01	380.8	44.90	7.00	A
WCM319-02	169.0	16.95	12.00	A
WCM319-03	141.6	13.70	13.00	A
WCM319-04	116.4	10.58	15.00	A
WCM319-05	83.5	7.20	18.00	A
WCM319-06	49.7	4.40	22.00	A
WCM319-07	41.5	3.83	24.00	A
WCM319-08	36.1	3.25	26.00	A
WCM319-09	29.3	2.83	28.00	A
WCM319-10	23.6	2.30	32.00	B
WCM319-11	18.6	1.90	37.00	B
WCM319-12	14.4	1.53	41.00	B
WCM319-13	10.4	1.28	45.00	B



Patent pending: Dartmouth and WCM

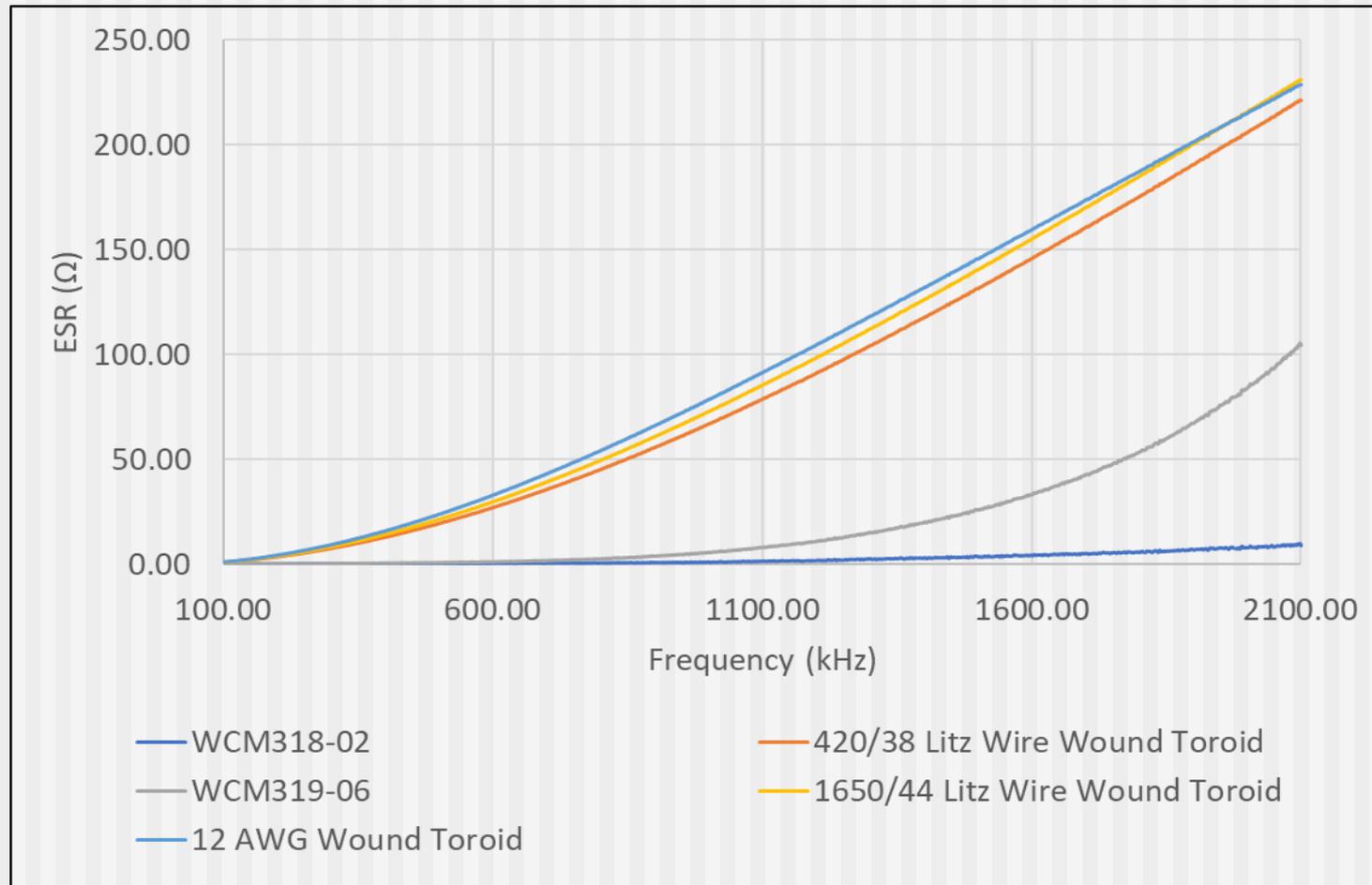
WCM Shaped Foil vs. Powdered Toroid

- Specs: 50 μ H, Max 10 amps RMS
- Toroid: Fe Al Si core
- WCM319 and WCM318 gapped ferrite

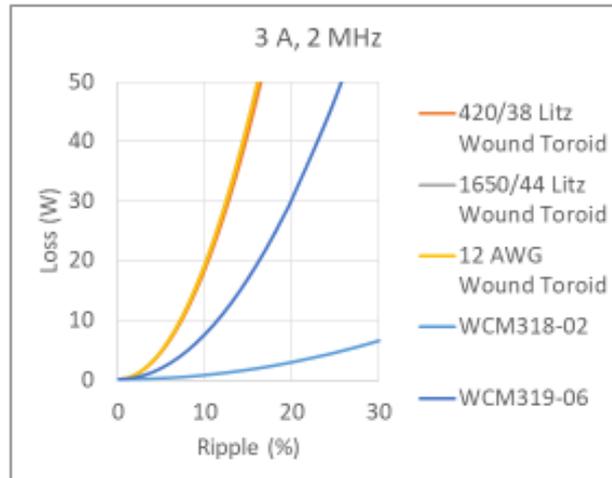
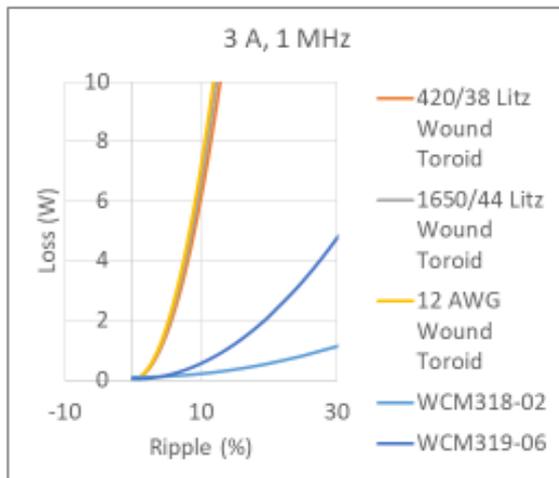
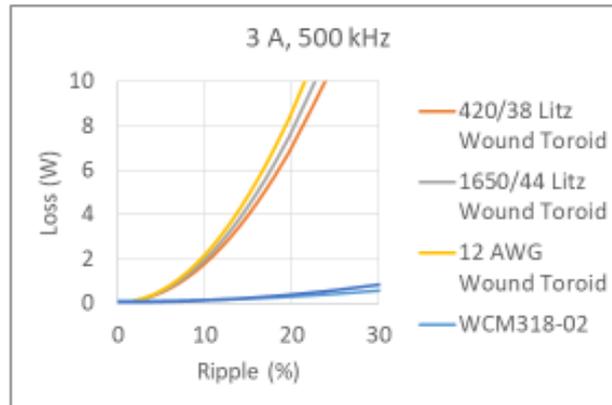
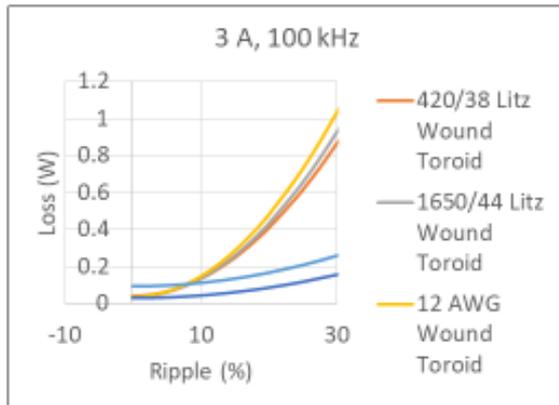


Design toroidal inductor to match inductance of WCM318, 319 and have the same DCR

ESR vs. Frequency

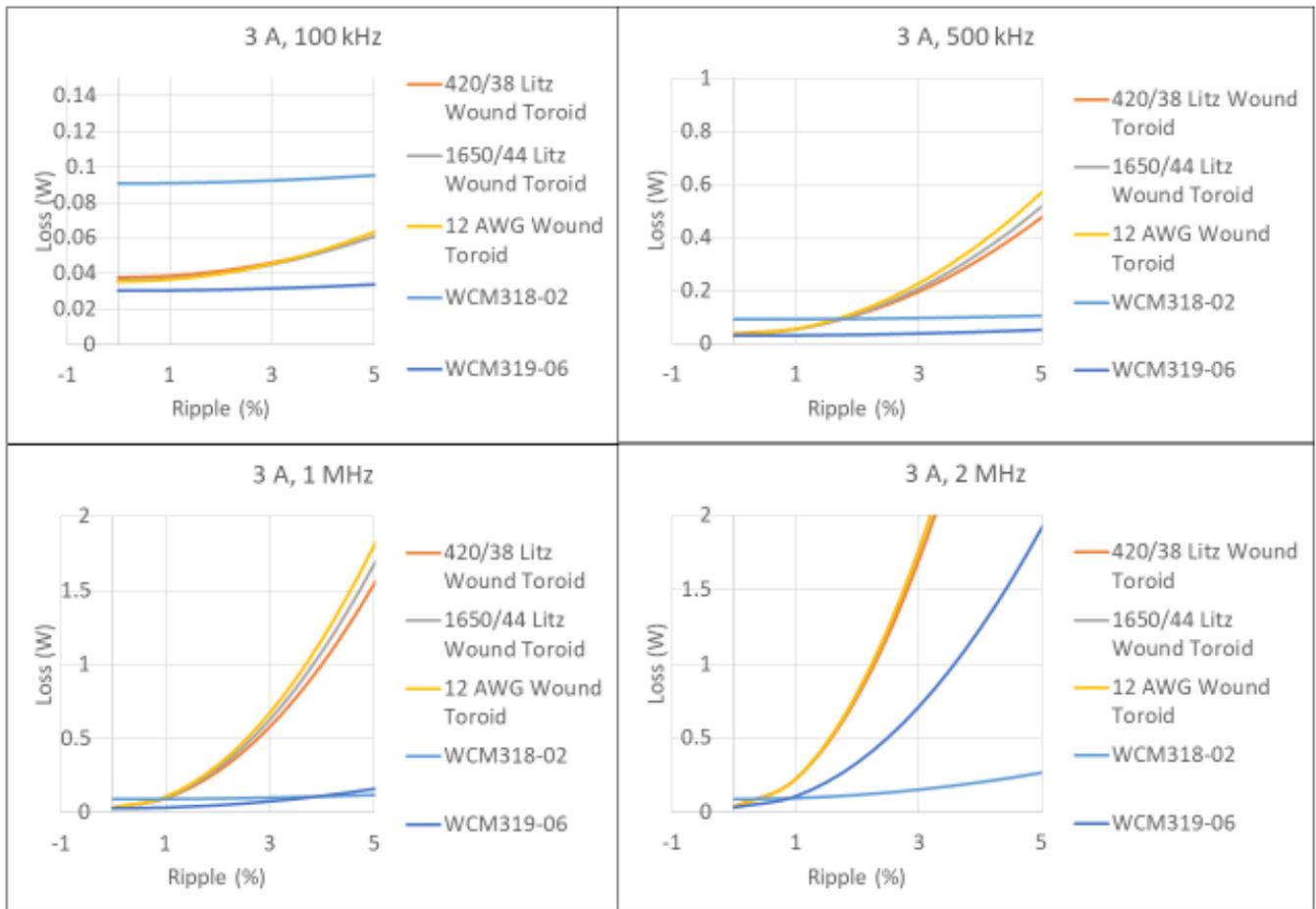


Loss vs. Ripple, no DC



As frequency increases, 318-02 becomes least lossy option despite higher DCR than other options.

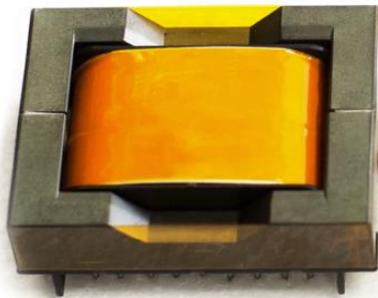
Loss vs. Ripple, Zoom to 5%



Comparison of 10 μH , 55 amp inductors



Shaped Foil



Iron Nickel Toroid



High Iron Toroid



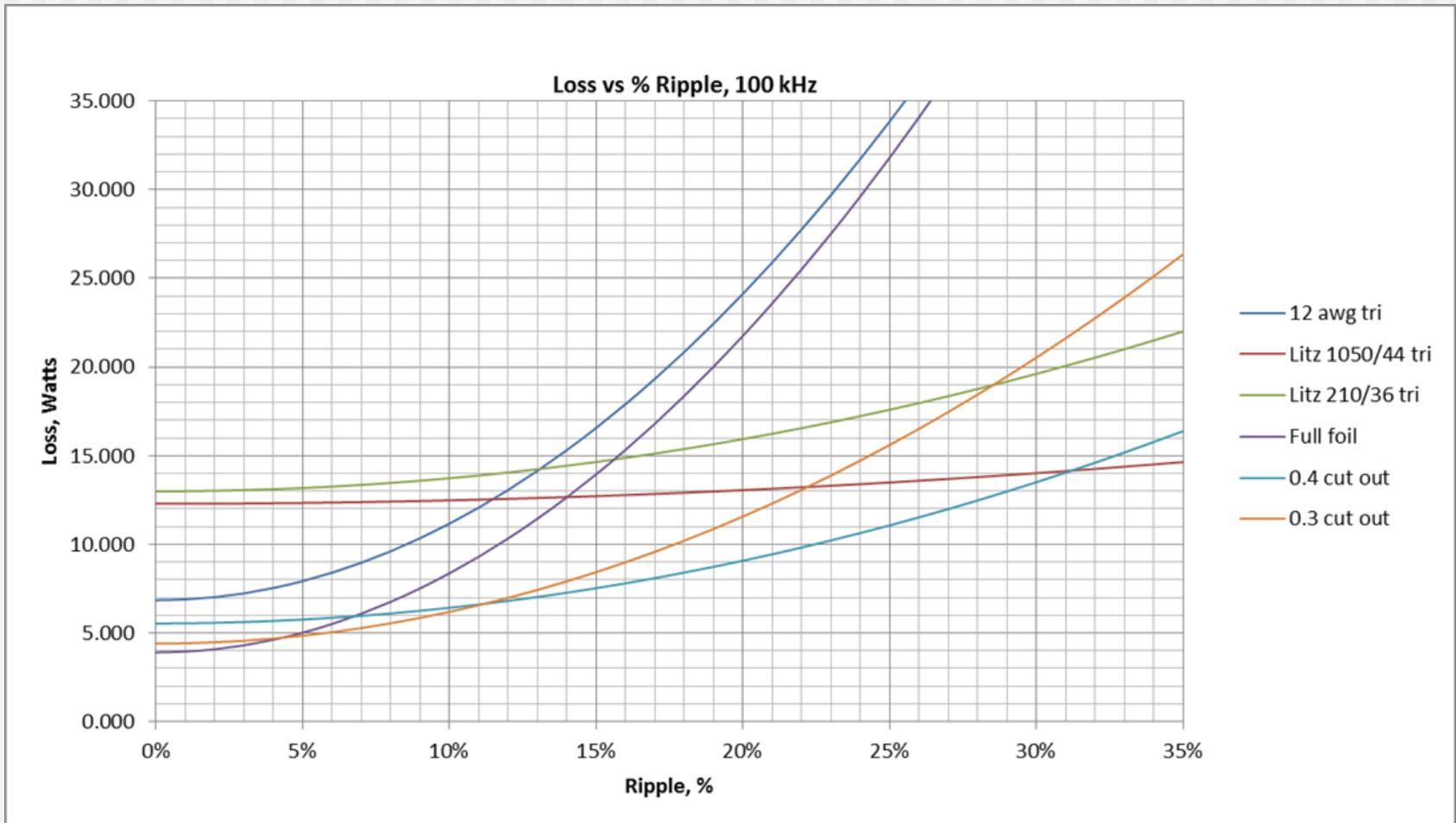
Helical Coil



Inductor Design	100 kHz losses (W)	250 kHz losses (W)	Total Volume (cm ³)	Weight (g)	Cost per Part (\$)
Shaped Foil	5.45	7.65	93.72	303.45	\$4.69
Iron Nickel Toroid	10.35	13.89	99.87	295.29	\$16.18
High Iron Toroid	14.19	16.40	130.65	475.59	\$9.48
22 Turn Helical	50.74	61.73	109.55	449.06	\$6.69
12 Turn Helical	15.67	27.28	109.55	447.92	\$6.66

Based on 2015 WCM study, copies available

Winding Loss: Gapped Ferrite



Cutout Patent issued: Dartmouth and WCM

Thank you for your time

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